



Siemens Matsushita Components

# Ferrites and Accessories

Design Parameters for Low-Distortion and Power Transformers  
TT/PR Cores

Preliminary Data Sheet

# Vakatseite

**1 Fundamentals for low-distortion transformers for digital data transmission (ISDN, xDSL)**

The new digital transmission technologies over copper like ISDN, HDSL (high-rate digital subscriber line) and ADSL (asymmetric digital subscriber line) require very small harmonic distortion in order to maintain maximal line length. This requirement can be calculated from material parameters for the third harmonic distortion with the Rayleigh model for small-signal hysteresis (sinusoidal current).

$$k_3 = \frac{u_3}{u_1} = 0,6 \cdot \tan \delta_h$$

$$= 0,6 \cdot \mu_e \cdot \eta_B \cdot \hat{B}$$

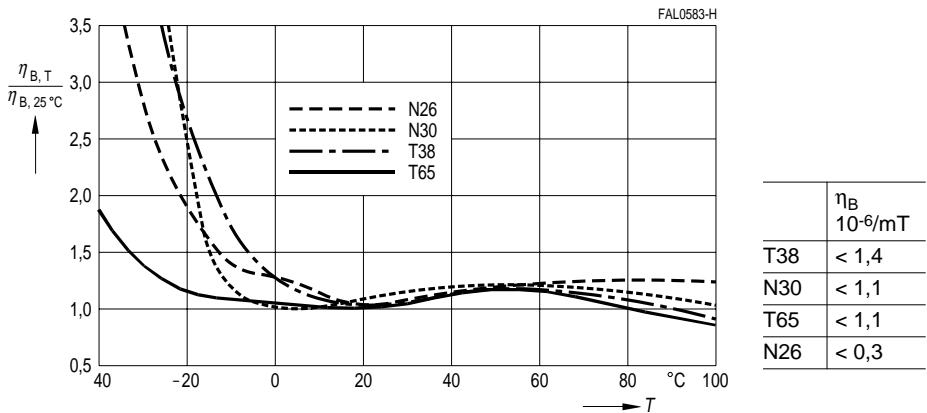
For a typical design a transformer has to be matched to a chipset via the turn ratios  $N1 : N2 : N3 \dots$ , the inductances  $L_1, L_2, L_3 \dots$  and the maximum dc resistances  $R_1, R_2, R_3 \dots$ .

The third harmonic distortion for winding j can then be calculated as

$$k_3 = \frac{0,6}{\mu_0} \cdot \underbrace{\eta_B}_{\text{Material}} \cdot \underbrace{\frac{\hat{U}}{2\pi f}}_{\text{Circuit conditions}} \cdot L_j \cdot \underbrace{\left[ \frac{\rho}{l_{Cu}} \sum_{j=1} \left( \frac{N_j}{N_1} \right)^2 \cdot \frac{1}{R_j} \right]^{3/2}}_{\text{Design constraints}} \cdot \underbrace{\frac{\sum_i I_i}{I_e} \cdot \frac{I_e}{A_e^2}}_{\text{Core Geometry}} \cdot \underbrace{\frac{I_N^{3/2}}{A_N^{3/2}}}_{\text{Coil former}}$$

This equation shows the contribution of the various design parameters:

a) The material is characterized by the hysteresis material constant  $\eta_B$ . Limit values for this parameter are given in the SIFERRIT material tables in the data book. The actual level for  $\eta_B$  varies for different cores. In order to select the best material for an application, the normalized temperature dependence  $\eta_B(T)/\eta_B(25^\circ\text{C})$  is of great help (see graph below). Being mainly composition-dependent, these curves are thus material-specific.



Normalized material hysteresis constant

b) The geometry can be taken into account by a core distortion factor (*CDF*) defined as

$$CDF = \frac{\sum l_i}{l_e} \cdot \frac{l_e}{A_e^2} \cdot \frac{l_N^{3/2}}{A_N^{3/2}}$$

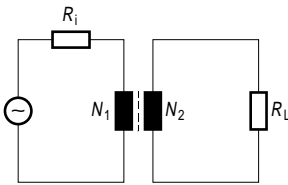
The factor  $\sum l_i / l_e$  is the closer to 1, the less the core section varies along the magnetic path (homogeneous core shape). For TT/PR cores without hole the factors are as follows:

TT/PR 14 × 8	<i>CDF</i> = 0,205 mm <sup>-4,5</sup>
TT/PR 18 × 11	<i>CDF</i> = 0,0561 mm <sup>-4,5</sup>
TT/PR 23 × 11	<i>CDF</i> = 0,0217 mm <sup>-4,5</sup>
TT/PR 23 × 18	<i>CDF</i> = 0,0119 mm <sup>-4,5</sup>
TT/PR 30 × 19	<i>CDF</i> = 0,00465 mm <sup>-4,5</sup>

$$CDF \sim \frac{1}{V_e^{3/2}}$$

I.e. the larger the core, the smaller is the distortion. Due to space restriction, however, the choice has to be made among the core shapes of a given size.

- c) The circuit conditions, i.e. voltage amplitude  $\hat{u}$  and frequency *f* affect directly the flux density in the core. For increasing flux density, a deviation of the absolute value of  $k_3$  from the calculated test value is expected, since the  $\tan \delta_h$  vs.  $\hat{B}$  curve deviates from linear.
- d) The distortion  $k_{3c}$  for a transformer in a circuit with given impedance conditions can be obtained from the following formula:



$$k_{3c} = \frac{k_3}{\sqrt{1 + \left[ 3\omega L_1 \cdot \left( \frac{1}{R_i} + \left( \frac{N_2}{N_1} \right)^2 \cdot \frac{1}{R_L} \right) \right]^2}}$$

- $R_i$  = internal resistance of generator
- $R_L$  = load resistance
- $L_1$  = primary inductance

The actual circuit distortion  $k_{3c}$  will in general be smaller than the calculated sinusoidal current value  $k_3$ .

**2 Power capacities**

In order to calculate the transmissible power, the following relationship is used (transformer with two equal windings):

$$P_{\text{trans}} = C \Delta B f A_e \cdot A_N \cdot j$$

where  $C$  is a coefficient characterizing the converter topology, i.e.

$C = 1$ : push-pull converter

$C = 0,71$ : single-ended converter

$C = 0,62$ : flyback converter

Both the core losses associated with the flux swing  $\Delta B$  and the copper losses due to the current density  $j$  result in a temperature increase  $\Delta T$ . Assuming that both loss contributions are equal and that  $P_V \sim B^2$ , the power capacity can be approximated by

$$P_{\text{trans}} \approx C \cdot \underbrace{\frac{PF}{\sqrt{P_V}}}_{\text{Material}} \cdot \underbrace{\frac{\Delta T}{R_{\text{th}}}}_{\text{Thermal design}} \cdot \underbrace{\sqrt{\frac{f_{\text{Cu}}}{\rho_{\text{Cu}}}}}_{\text{Winding}} \cdot \underbrace{\sqrt{\frac{A_N \cdot A_e}{I_N \cdot I_e}}}_{\text{Geometry}}$$

The equation shows how the different aspects in the design contribute to the power capacity:

- a) The material term is the performance factor ( $PF = f \cdot B_{\text{max}}$ ) divided by the square root of the specific core loss level for which it was derived. For a given core shape deviations from this value are possible as given by its data sheet.
- b) The values for  $\Delta T$  are associated with the material according to the following table.

	$\Delta T_{\text{max}}$ K
N87	50
N49	20
N59	30
N27	30

For actual designs the actual values for  $R_{\text{th}}$  should be determined and the tabulated  $P_{\text{trans}}$  values adjusted accordingly.

- c) The winding design was taken into account in the calculations by  $f_{\text{Cu}} = 0,4$  and  $\rho_{\text{Cu}}$  for DC. In actual design large deviations of the dc resistance due to high frequency effects (skin effect, proximity effect) occur, unless special wire types such as litz wires are used. If the  $R_{\text{AC}}/R_{\text{DC}}$  ratio for a given winding is known, this can be used to correct the tabulated power capacities accordingly.
- d) The geometry term is related to the core shape and size. However, note that the thermal resistance is also size-dependent via the empirical relation:

$$R_{\text{th}} \sim \frac{1}{\sqrt{V_e}}$$

The tabulated power capacities provide a means for making a selection among cores, although the absolute values will not be met in practice for the reasons explained before.

**Power capacities of TT/PR cores**

Core	$R_{th}$	$\sqrt{\frac{A_N \cdot A_e}{I_N \cdot I_e}}$	$P_{trans}$ (N87/100 kHz) Wound transformer
	K/W	mm	W
TT/PR 14 × 8	77	0,596	52
TT/PR 18 × 11	54	0,815	114
TT/PR 23 × 11	39	1,000	204
TT/PR 23 × 18	31	1,135	297
TT/PR 30 × 19	24	1,435	500

- Also available with center hole
- Types with special  $A_L$  value on request
- TT/PR cores are supplied in sets
- Coil formers available on request

**Magnetic characteristics** (per set)

$$\Sigma l_e/A_e = 0,84 \text{ mm}^{-1}$$

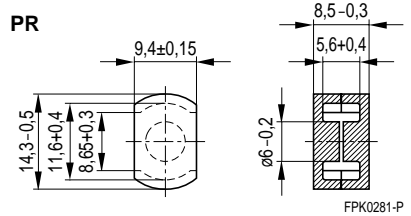
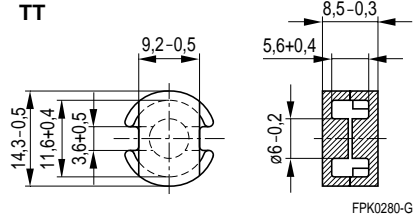
$$l_e = 25,3 \text{ mm}$$

$$A_e = 25,3 \text{ mm}^2$$

$$A_{\min} = 22,1 \text{ mm}^2$$

$$V_e = 539 \text{ mm}^3$$

**Approx. weight** TT 3,5 g/set  
PR 3,2 g/set



**Ungapped <sup>1)</sup>**

Material	$A_L$ value nH	$\mu_e$	$A_{L1\min}$ nH	$P_V$ W/set	Ordering code	Type
N87	2000 + 30/- 20 %	1340	1350	< 0,35 (200 mT, 100 kHz, 100 °C)	B65754-J-R87 B65755-J-R87	TT PR
N26	2000 + 30/- 20 %	1400			B65754-J-R26 B65755-J-R26	TT PR
N30	4000 + 30/- 20 %	2680			B65754-J-R30 B65755-J-R30	TT PR
T65	5200 + 30/- 20 %	3480			B65754-J-R65 B65755-J-R65	TT PR
T38	8500 + 40/- 30 %	5695			B65754-J-Y38 B65755-J-Y38	TT PR

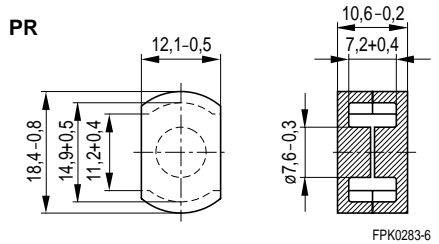
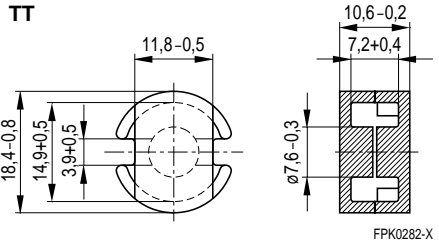
1) Preliminary data

- Also available with center hole
- Types with special  $A_L$  value on request
- TT/PR cores are supplied in sets
- Coil formers available on request

**Magnetic characteristics** (per set)

$\Sigma l_e/A_e = 0,68 \text{ mm}^{-1}$   
 $l_e = 27,3 \text{ mm}$   
 $A_e = 40,3 \text{ mm}^2$   
 $A_{\min} = 36,0 \text{ mm}^2$   
 $V_e = 1100 \text{ mm}^3$

**Approx. weight** TT 6,4 g/set  
PR 6,2 g/set



**Unapped** <sup>1)</sup>

Material	$A_L$ value nH	$\mu_e$	$A_{L1\min}$ nH	$P_V$ W/set	Ordering code	Type
N87	2800 + 30/- 20 %	1510	1670	< 0,7 (200 mT, 100 kHz, 100 °C)	B65756-J-R87 B65757-J-R87	TT PR
N26	2600 + 30/- 20 %	1400			B65756-J-R26 B65757-J-R26	TT PR
N30	5000 + 30/- 20 %	2695			B65756-J-R30 B65757-J-R30	TT PR
T65	7200 + 30/- 20 %	3880			B65756-J-R65 B65757-J-R65	TT PR
T38	10800 + 40/- 30 %	5820			B65756-J-Y38 B65757-J-Y38	TT PR

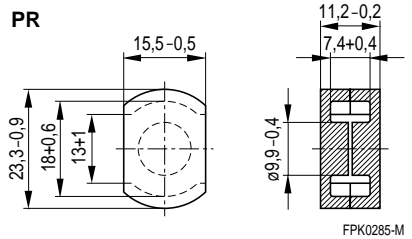
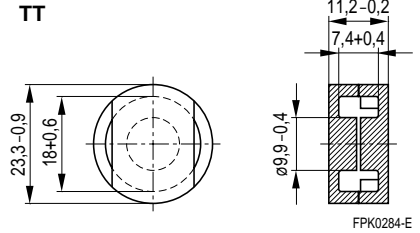
<sup>1)</sup> Preliminary data

- Also available with center hole
- Types with special  $A_L$  value on request
- TT/PR cores are supplied in sets
- Coil formers available on request

**Magnetic characteristics** (per set)

$\Sigma l_e/A_e = 0,45 \text{ mm}^{-1}$   
 $l_e = 31,2 \text{ mm}$   
 $A_e = 68,8 \text{ mm}^2$   
 $A_{\min} = 62,8 \text{ mm}^2$   
 $V_e = 2144 \text{ mm}^3$

**Approx. weight** TT 13,8 g/set  
PR 11,4 g/set



**Ungapped <sup>1)</sup>**

Material	$A_L$ value nH	$\mu_e$	$A_{L1\min}$ nH	$P_V$ W/set	Ordering code	Type
N87	4800 + 30/- 20 %	1730	2500	1,4 (200 mT, 100 kHz, 100 °C)	B65716-L-R87 B65738-L-R87	TT PR
N26	4400 + 30/- 20 %	1590			B65716-L-R26 B65738-L-R26	TT PR
N30	7900 + 30/- 20 %	2850			B65716-L-R30 B65738-L-R30	TT PR
T65	11800 + 30/- 20 %	3880			B65716-L-R65 B65738-L-R65	TT PR
T38	16400 + 40/- 30 %	5920			B65716-L-Y38 B65738-L-Y38	TT PR

1) Preliminary data

- Also available with center hole
- Types with special  $A_L$  value on request
- TT/PR cores are supplied in sets
- Coil formers available on request

**Magnetic characteristics** (per set)

$$\Sigma l_e/A_e = 0,62 \text{ mm}^{-1}$$

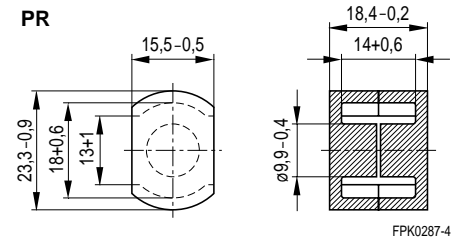
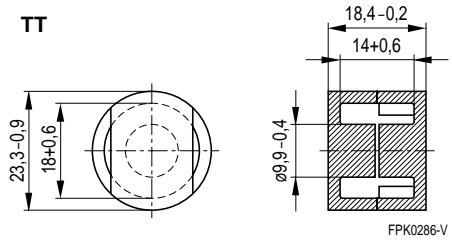
$$l_e = 45,1 \text{ mm}$$

$$A_e = 73,1 \text{ mm}^2$$

$$A_{\min} = 67,4 \text{ mm}^2$$

$$V_e = 3293 \text{ mm}^3$$

**Approx. weight** TT 20,6 g/set  
PR 16,6 g/set



**Unapped** <sup>1)</sup>

Material	$A_L$ value nH	$\mu_e$	$A_{L1\min}$ nH	$P_V$ W/set	Ordering code	Type
N87	3800 + 30/- 20 %	1870	1830	< 2,2 (200 mT, 100 kHz, 100 °C)	B65716-J-R87 B65738-J-R87	TT PR
N26	3600 + 30/- 20 %	1770			B65716-J-R26 B65738-J-R26	TT PR
N30	6500 + 30/- 20 %	3190			B65716-J-R30 B65738-J-R30	TT PR
T65	9200 + 30/- 20 %	4520			B65716-J-R65 B65738-J-R65	TT PR
T38	13800 + 40/- 30 %	6770			B65716-J-Y38 B65738-J-Y38	TT PR

<sup>1)</sup> Preliminary data

- Also available with center hole
- Types with special  $A_L$  value on request
- TT/PR cores are supplied in sets
- Coil formers available on request

**Magnetic characteristics** (per set)

$$\Sigma l_e/A_e = 0,39 \text{ mm}^{-1}$$

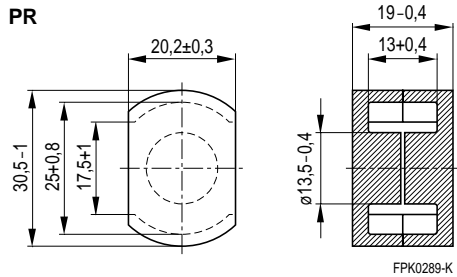
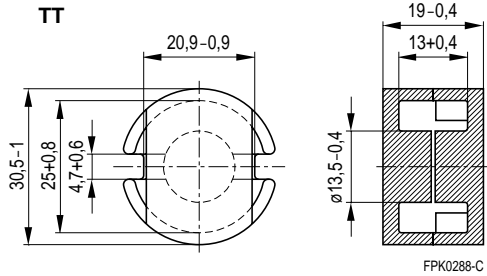
$$l_e = 46,4 \text{ mm}$$

$$A_e = 119 \text{ mm}^2$$

$$A_{\min} = 99,4 \text{ mm}^2$$

$$V_e = 5534 \text{ mm}^3$$

**Approx. weight** TT 33,3 g/set  
PR 29,6 g/set



**Ungapped <sup>1)</sup>**

Material	$A_L$ value nH	$\mu_e$	$A_{L1\min}$ nH	$P_V$ W/set	Ordering code	Type
N87	5400 + 30/- 20 %	1680	2900	< 2,8 (200 mT, 100 kHz, 100 °C)	B65730-J-R87 B65735-J-R87	TT PR
N26	5900 + 30/- 20 %	1830			B65730-J-R26 B65735-J-R26	TT PR
N30	9400 + 30/- 20 %	2920			B65730-J-R30 B65735-J-R30	TT PR
T65	14000 + 30/- 20 %	4340			B65730-J-R65 B65735-J-R65	TT PR
T38	22800 + 40/- 30 %	7075			B65730-J-Y38 B65735-J-Y38	TT PR

<sup>1)</sup> Preliminary data

**Published by Siemens Matsushita Components GmbH & Co. KG  
Marketing Kommunikation, Postfach 80 17 09, D-81617 München**

© Siemens Matsushita Components 1998. All Rights Reserved.

As far as patents or other rights of third parties are concerned, liability is only assumed for components per se, not for applications, processes and circuits implemented within components or assemblies.

The information describes the type of component and shall not be considered as assured characteristics.

Terms of delivery and rights to change design reserved.

This brochure replaces the previous edition.

For questions on technology, prices and delivery please contact the Sales Offices of Siemens AG, Passive Components and Electron Tubes Group, in the Federal Republic of Germany or the international Siemens Companies and Representatives.

Due to technical requirements components may contain dangerous substances. For information on the type in question please also contact one of our Sales Offices.